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# Phasing Skin Factor Analysis for Oil Wells Completions

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### Abstract

This paper presents a comparative analysis of the effect induced by perforation skin in case of vertical production oil wells. The Karakas and Tariq method has been used, by applying it both to the classic perforation system and to the one developed by Penetrator Canada Inc.

Key words: skin, phasing skin, producing well system, MaxPerf

### **Calculation of the Skin Effect**

For calculation of perforation skin, according to perforations type, we used a simple and accurate semi-analytical method introduced and developed by Karakas and Tariq (1988, 1991) for perforated systems.

In this method it is assumed that perforation skin is the summation of horizontal, vertical, wellbore and perforation crush skin:

$$S_{perf} = S_H + S_V + S_{Wb} + S_C \tag{1}$$

Figure 1 gives all the relevant variables to calculate the perforation skin. These include the well radius  $(r_w)$ , the perforation radius  $(r_{perf})$ , the perforation length  $(l_{perf})$ , the angle of perforation phasing ( $\alpha$ ) and the vertical distance between two successive perforations  $(h_{perf})$ .

# Horizontal Skin, S<sub>H</sub>

The horizontal skin is:

$$s_H = \ln \frac{r_w}{r_w(\alpha)} \tag{2}$$

where  $r_w(\alpha)$  is the effective wellbore radius and it is a function of phase angle,  $\alpha$ .

$$\dot{r}_w(\alpha) = a_\alpha \cdot l_{perf}, \alpha = 0(360^\circ)$$
(3)

$$r_w(\alpha) = a_\alpha (r_w + l_{perf}), \alpha \neq 0(360^\circ)$$
<sup>(4)</sup>

The constant  $a_{\alpha}$  depends on the perforation phasing (Table 1). The total contribution of the horizontal skin is usually small.

α	aα	<b>a</b> <sub>1</sub>	<b>a</b> <sub>2</sub>	<b>b</b> <sub>1</sub>	<b>b</b> <sub>2</sub>	<b>c</b> <sub>1</sub>	<b>c</b> <sub>2</sub>
0	0.25	-2.091	0.0453	5.1313	1.8672	0.16000	2.675
180	0.5	-2.025	0.0943	3.0373	1.8115	0.02600	4.532
120	0.648	-2.018	0.0634	1.6136	1.777	0.00660	5.32
90	0.726	-1.905	0.1038	1.5674	1.6935	0.00190	6.155
60	0.813	-1.898	0.1023	1.3654	1.649	0.00030	7.509
45	0.86	-1.788	0.2398	1.1915	1.6392	0.00005	8.791

 Table 1. Constant for perforation skin effect [3]

# Vertical Skin, S<sub>V</sub>

The vertical skin effect is:

where:

$$s_V = 10^a h_D^{b-1} r_D^b$$
 (5)

$$h_D = \frac{r_{perf}}{l_{perf}} \sqrt{\frac{k_H}{k_V}}$$
(6)

$$r_{D} = \frac{r_{perf}}{2h_{perf}} \left( 1 + \sqrt{\frac{k_{H}}{k_{V}}} \right)$$
(7)

$$a = a_1 \log r_D + a_2; \ b = b_1 \log r_D + b_2 \tag{8}$$

and  $k_H$ ,  $k_V$  are the horizontal and vertical permeabilities.

The vertical skin effect has the largest contribution for total perforation skin and takes important values according to perforation densities and radius.

# Wellbore Skin, S<sub>Wb</sub>

For wellbore skin effect, the calculation formula is:

$$s_{wb} = c_1 e^{c_2 r_{wb}} (9)$$

where

$$r_{wb} = \frac{r_w}{l_{perf} + r_w} \tag{10}$$

is an dimensionless factor; the constants  $c_1$  and  $c_2$  can also be taken from Table 1.

# Perforation Crush Skin, S<sub>C</sub>

This skin effect has an important contribution to total perforating skin effect; it is well highlighted in Figure 2 and it can be calculated with the following equation:

$$s_{C} = \frac{h_{perf}}{l_{perf}} \left(\frac{k_{H}}{k_{C}} - 1\right) \ln \frac{r_{c}}{r_{perf}}$$
(11)

where  $k_C$  is crushed zone permeability and  $r_C$  is the distance from the center of perforation to the edge of crushed zone.

#### **MaxPERF** Penetration System

**Penetrators Canada Inc.** has developed completion and stimulation systems that provide a more efficient method to establish the communication between the wellbore and the target zone. **MaxPERF** tool system (fig. 3) can be run in new or existing well to drill multiple radial tunnels in the formation, up to 1.8 m laterally from the wellbore and 25.4 mm diameter.



Fig. 1. Well variables for perforation skin [3]



Fig. 2. Crushed and damaged zone



Fig. 3. MaxPERF Tool [7]

# Application

# Well "A" Data (Standard penetration)

- Well Radius,  $r_w = 0.07$  m
- Perf Length,  $l_{perf} = 0.152 \text{ m}$
- Perforation Spacing,  $h_{perf} = 0.166$  m
- Perforation Radius,  $r_{perf} = 6.35$  mm
- Shot Density = 6 SPM
- Crushed Zone Radius,  $r_c=12.7$  mm

### Well "B" Data (MaxPERF penetration)

- Well Radius,  $r_w = 0.07$  m
- Perf Length,  $l_{perf} = 1 \text{ m}$
- Perforation Spacing,  $h_{perf} = 0.166 \text{ m}$
- Perforation Radius,  $r_{perf} = 12,7 \text{ mm}$
- Shot Density = 6 SPM
- Crushed Zone Radius,  $r_c = 0 \text{ mm}$

k/k	$\alpha = 360^{\circ}$	$\alpha = 180^{\circ}$	$\alpha = 120^{\circ}$	$\alpha = 90^{\circ}$	$\alpha = 60^{\circ}$	$\alpha = 45^{\circ}$		
κγικΗ	Sperf							
1	2.35	1.51	1.56	1.41	1.63	1.59		
0.8	2.54	1.76	1.83	1.65	1.88	1.83		
0.6	2.87	2.13	2.22	1.99	2.26	2.17		
0.4	3.42	2.74	2.85	2.54	2.84	2.71		
0.2	4.66	4.06	4.21	3.68	4.06	3.81		

**Table 2.** Perforation skin effect vs. permeability anisotropy  $(k_V/k_H)$  and phase angle



**Fig. 4.** Perforation skin effect vs.  $k_V/k_H$  and phase angle

	Standard perforations							MaxPerf	
α	$k_c = k_H$		$k_c = 0.1 k_H$		$k_c = 0.01 \text{ k}_{\text{H}}$		$L_{perf} = 1m$ $r_{perf} = 12.7mm$		
	$k_{H}/k_{V} = 10$	$k_H/k_V = 1$	$k_{H}/k_{V} = 10$	$k_H/k_V = 1$	$k_{H}/k_{V} = 10$	$k_H/k_V = 1$	$k_{H}/k_{V} = 10$	$k_H/k_V = 1$	
	$S_{perf}$	Sperf	Sperf	Sperf	Sperf	Sperf	$S_{perf}$	Sperf	
360°	6.42	2.32	13.26	9.16	81.6	77.5	-0.6	-1	
180°	5.87	1.51	12.7	8.35	81.1	76.7	-1.19	-1.8	
120°	6.02	1.56	12.85	8.4	81.2	76.8	-1.2	-1.97	
90°	5.15	1.41	11.97	8.25	80.3	76.6	-1.25	-2.02	
60°	5.6	1.63	12.42	8.46	80.8	76.8	-1.14	-2.04	
45°	5.19	1.59	12	8.43	80.4	76.8	-1.12	-2.03	

**Table 3.** Perforation skin effect vs.  $k_H/k_V$ , phase angle and crushed zonefor Standard and MaxPerf perforations



Fig. 5. Perforation skin effect vs. phase angle for different crush zone permeabilities

### Conclusions

Both phasing skin and permeability anisotropy have a major influence to Total well Skin Factor. The crush zone made by perforated system also increases the skin factor four times (see fig. 5).

By using MaxPerf Penetrating System, the crush zone will be eliminated, the perforated length will be 1m instead of 0.152 - 0.203 m and also the total well skin factor will reach negative values (see fig. 6).

This analysis indicates that the smallest phasing skin was recorded for phase angle =  $90^{\circ}$  (see figs. 6 and 7) regardless of the perforated system used.



Fig. 6. Perforation skin effect for Standard and MaxPerf perforations



Fig. 7. Perforation skin effect vs. phase angle

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# Rezumat

În această lucrare este prezentată o analiză detaliată, în cazul a două sonde de țiței, a influenței modului de perforare asupra factorului skin. S-a utilizat metoda semi-analitică Karakas și Tariq, aplicată atât sistemului de perforare clasic, cât și modului de deschidere a stratelor productive dezvoltat de Penetrator Canada Inc.