

# RESEARCH ON THE SIMULATION OF THE OPERATION OF ROBOTIC MECHANISMS

Georgeta Toma <sup>1</sup> 问

<sup>1</sup> Petroleum-Gas University of Ploiesti, Romania e-mail: georgeta.toma@upg-ploiesti.ro

#### DOI: 10.51865/JPGT.2024.02.15

## ABSTRACT

The optimal design of the structures from the component of the robotic mechanisms requires a good knowledge of the various parameters during their operation. Among them are mentioned the working parameters that give the position, speed and acceleration at the operational level of the robots, as well as at the level of the active joints from the component of the robotic mechanisms. This paper presents how a functional simulator of robotic active mechanisms called *RobSim* was created. The simulator allows the positional and kinematic analysis of active robotic mechanisms, regardless of their configuration and the number of component modules. The positional analysis is performed parametrically. A polynomial variation of the fifth degree was considered for the position parameters at the level of active joints. The simulator allows establishing the position and orientation at the operational level of the analyzed robotic mechanism, as well as the trajectory followed by the robot during operation. Also, the simulator allows establishing the speeds and accelerations both at the operational level of the robotic mechanisms, as well as at the level of the active joints in their component.

Keywords: industrial robots, mechanism, active joints, position parameters, kinematics

#### INTRODUCTION

The simulation of the operation of robotic mechanisms represents an always current field of study due to the results offered, absolutely necessary in the correct evaluation of the operation of robots in the performance of various tasks [1-10]. In this context, the precise establishment of the position at the operational level of the industrial robots during the performance of tasks and the distribution of speeds and accelerations at this level is very important in the optimization of work cycles [11-23]. Likewise, simulating the operation of robots at the level of active joints considering different variation functions for the motor coordinates is equally important.

The scope of this paper is to present how a functional simulator of robotic active mechanisms can be created. The method chosen in the realization of the simulator, by using the special symbolic calculation capabilities of the Maple program [24, 25], introduces a novelty character and offers it multiple possibilities of obtaining results in numerical and symbolic form. The simulator called *RobSim* allows the positional and kinematic analysis of active robotic mechanisms, regardless of their configuration and the number of component modules. It allows establishing the position and orientation at



the operational level of the analyzed robotic mechanism, as well as the trajectory followed by the robot during operation. Also, the simulator allows establishing the speeds and accelerations both at the operational level of the robotic mechanisms, as well as at the level of the active joints in their component.

# THEORETICAL CONSIDERATIONS AND RESULTS OF THE SIMULATIONS

Within the positional analysis of the active robotic mechanisms, the determination of the relative position and orientation between the component modules during operation, as well as the position and orientation of the final effector in relation to the base system of coordinates of the robotic mechanism is performed parametrically [8,11]. Figure 1 shows the four parameters (the angle  $\alpha_{i+1}$ , the distance  $d_{i+1}$ , the angle  $\theta_{i+1}$  and the distance  $r_{i+1}$ ) that define the relative position and orientation between two consecutive modules from the component of an active robotic mechanism.

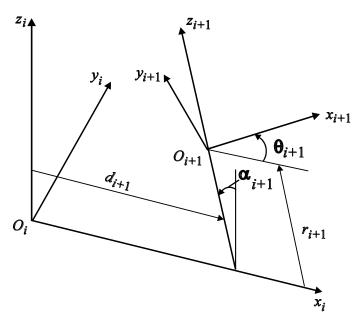


Figure 1. The systems of coordinates attached to two consecutive modules

The homogeneous transformation that establishes the relative position and orientation between consecutive modules i and i+1 has the following expression [8]:

$${}^{i}T_{i+1} = \begin{bmatrix} \cos\theta_{i+1} & -\sin\theta_{i+1} & 0 & d_{i+1} \\ \cos\alpha_{i+1} \cdot \sin\theta_{i+1} & \cos\alpha_{i+1} \cdot \cos\theta_{i+1} & -\sin\alpha_{i+1} & -r_{i+1} \cdot \sin\alpha_{i+1} \\ \sin\alpha_{i+1} \cdot \sin\theta_{i+1} & \sin\alpha_{i+1} \cdot \cos\theta_{i+1} & \cos\alpha_{i+1} & r_{i+1} \cdot \cos\alpha_{i+1} \\ 0 & 0 & 0 & 1 \end{bmatrix}$$
(1)

The *RobSim* simulator demands the number of component modules of the analyzed robot must to be entered first, and then are required the parameters corresponding to the relative position and orientation between the consecutive modules.



The position and orientation at the operational level of the robot is established with the relation:

$${}^{0}T_{T} = {}^{0}T_{n} \cdot {}^{n}T_{T} \tag{2}$$

where:

$${}^{0}T_{n} = {}^{0}T_{1} \cdot {}^{1}T_{2} \cdot \dots \cdot {}^{n-1}T_{n}$$
(3)

and then the elements of the homogeneous transformation  ${}^{n}T_{T}$  must be introduced in the simulator according to the way in which the coordinates system attached to the terminal module and the one attached to the final effector of the robot were chosen.

The *RobSim* simulator allows obtaining results both in symbolic and numerical form. For the numerical simulations, it was considered that the coordinates at the motor axle level vary according to the following law:

$$q(t) = q_i + g(t) \cdot (q_f - q_i) \tag{4}$$

where:  $q_i$  and  $q_f$  represent the initial and the final value of the active joint coordinate q.  $q_i$  and  $q_f$  are demanded to be introduced for any active component joint.

g(t) is a polynomial function of time of degree five:

$$g(t) = 10 \cdot \left(\frac{t}{t_f}\right)^3 - 15 \cdot \left(\frac{t}{t_f}\right)^4 + 6 \cdot \left(\frac{t}{t_f}\right)^5$$
(5)

In relation (5),  $t_f$  represents the time interval in which the simulation of the analyzed robot is carried out.

The *diff* function from the Maple program was used to determine the speed and acceleration variation both at the level of the motor axes and at the operational level of the analyzed robot.

A series of results obtained by running the *RobSim* simulator in the case of the robot with five rotation modules in Figure 2 are presented below.

In this case 
$$\theta_i = q_i; i = \overline{1,5}$$
; the values for the angles  $\alpha_i, i = \overline{1,5}$ , are:  $0, -\frac{\pi}{2}, 0, 0$  and  $-\frac{\pi}{2}$ ;

the distances  $d_i$ ,  $i = \overline{1,5}$ , are as follows:  $0, 0, l_2, l_3$  and 0 and the distances  $r_i$ ,  $i = \overline{1,5}$ , are all equal to zero.

The expression of the homogeneous transformation  ${}^{5}T_{T}$  is in this case:

$${}^{5}T_{T} = \begin{bmatrix} -1 & 0 & 0 & 0 \\ 0 & -1 & 0 & 0 \\ 0 & 0 & 1 & l_{4} \\ 0 & 0 & 0 & 1 \end{bmatrix}$$
(6)



The initial and the final values of the active joint coordinates,  $q_i$  and  $q_f$ , introduced in

this simulation case are:  $0, -\frac{\pi}{2}, \frac{\pi}{2}, -\frac{\pi}{2}, 0$  and  $\frac{\pi}{3}, -\frac{\pi}{6}, \frac{\pi}{3}, -\frac{\pi}{3}, \frac{\pi}{4}$ , respectively.

In the representation of the systems of coordinates attached to the component modules of the robot, the *y* axes were omitted because they do not intervene in the evaluation of the parameters.

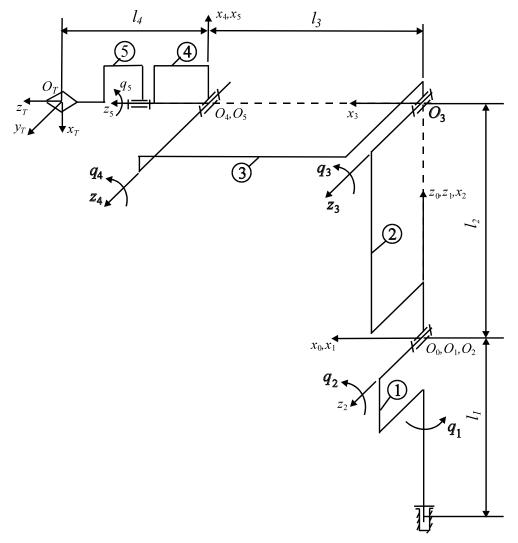


Figure 2. Robot mechanism with five rotation modules

The simulation was carried out for a time interval  $t_f = 10 s$ . The following values were considered for the dimensions of the component modules:  $l_1 = 0.55 \text{ m}$ ;  $l_2 = 0.42 \text{ m}$ ;  $l_3 = 0.34 \text{ m}$  and  $l_4 = 0.15 \text{ m}$ .

Figure 3 shows the variation curves of the coordinates of the characteristic point  $O_T$  in relation to the fixed system of coordinates  $O_0 x_0 y_0 z_0$ .

Figure 4 shows the trajectory followed by the characteristic point  $O_T$ .



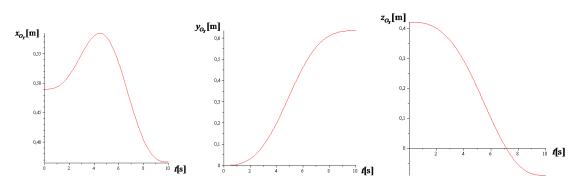
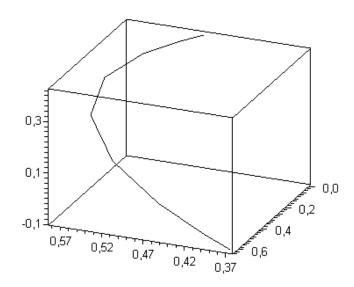


Figure 3. The variation curves of the coordinates of the characteristic point  $O_T$ 



**Figure 4.** The trajectory followed by the characteristic point  $O_T$ 

Figure 5 shows the variation curves of the derivatives in relation to time of the coordinates of the characteristic point  $O_T$  in relation to the fixed system of coordinates  $O_0 x_0 y_0 z_0$ . Figure 6 shows the variation curve of the speed of characteristic point  $O_T$ .

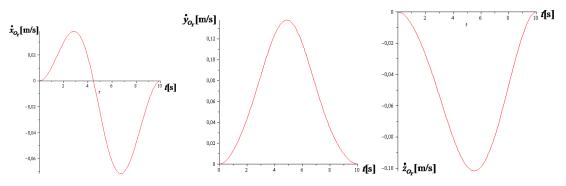
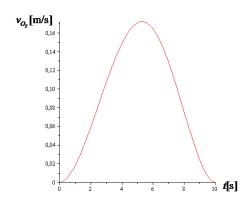


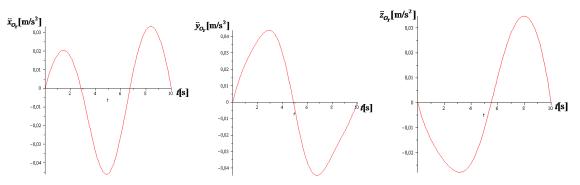
Figure 5. The variation curves of the derivatives in relation to time of the coordinates of the characteristic point  $O_T$ 





**Figure 6.** The variation curve of the speed of characteristic point  $O_T$ 

In Figure 7 are represented the variation curves for  $\ddot{x}_{o_T}$ ,  $\ddot{y}_{o_T}$  and  $\ddot{z}_{o_T}$  and Figure 8 shows the variation curve of the acceleration of characteristic point  $O_T$ .



**Figure 7.** The variation curves of  $\ddot{x}_{o_{\tau}}, \ddot{y}_{o_{\tau}}$  and  $\ddot{z}_{o_{\tau}}$ 

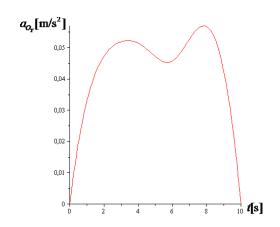


Figure 8. The variation curve of the acceleration of characteristic point  $O_T$ 

#### CONCLUSIONS

In this article, the stages of creating a simulator with the help of which the active mechanisms of industrial robots can be analyzed positionally and kinematically were presented. The positional analysis was performed parametrically, and in the kinematic analysis it was considered that the positional parameters at the level of active joints have



a polynomial variation of the fifth degree. In the realization of the simulator, called *RobSim*, the special symbolic calculation capabilities of the Maple program were used, so that the results can be obtained both in symbolic and numerical form. The simulator was run in the case of a robotic mechanism with five rotation modules. It was established the position and orientation at the operational level of the analyzed robotic mechanism, as well as the trajectory followed by the robot during operation. Also, it were determined the speeds and accelerations at the operational level of this robotic mechanism, as well as at the level of the active joints. Finally, it can be concluded that the *RobSim* simulator is useful to all those involved in the field of robotics, the results that can be obtained with it being necessary to establish optimal structures of robotic mechanisms.

## REFERENCES

- [1] Nae I., Bădoiu D., Toma G., On the establishment and visualization of the multiple configurations of the Mitsubishi RV-1A robot system, Petroleum-Gas University of Ploiesti Bulletin, Technical Series, Volume 66, Issue 1, p. 73-78, 2014;
- [2] Bădoiu D., On the movement equation of the quadrilateral mechanism, Buletinul Universitatii Petrol-Gaze din Ploiesti, Seria Tehnica, Vol. 67, No. 2, pp. 67-72, 2015;
- [3] Bădoiu D., Toma G., *Research on designing a multiloop planar linkage*, IOP Conference Series: Materials Science and Engineering, Volume 659, Issue 1, pp. 1-9, 2019;
- [4] Bădoiu D., On the calculus of the equilibrium moment for a mechanism with three independent contours, Buletinul Universitatii Petrol-Gaze din Ploiesti, Seria Tehnica, Vol. 67, No. 1, pp. 99-104, 2015;
- [5] Bădoiu D., Petrescu M., Toma G., Helthuis J.C., *On the generation of complex trajectories using a robotic system with six degrees of freedom*, Applied Mechanics and Materials, Vol. 657, p. 803-807, 2014
- [6] Vasilescu S., Bădoiu D., *Research Concerning the Variation of the Motor Moment in the Case of a Plane Mechanism*, Buletinul Universitatii Petrol-Gaze din Ploiesti, Seria Tehnica, Vol 63, No. 3, pp. 1-4, 2011;
- [7] Tudor I., Rîpeanu R.G., Bădoiu D., Device and simulator for testing pairs of materials used for joints design, Proceedings of the 2nd International Conference on Manufacturing Engineering ICMEN and EUREKA Brokerage Event, pp. 417-423, Grecia, 2005;
- [8] Bădoiu D., Mecanica Roboților, Editura Universitatii Petrol-Gaze din Ploiesti, 2006
- Bădoiu D., Research concerning the dynamics of a manipulator robot with elastic links, Proceedings of International Symposium of the Institute of Solid Mechanics SISOM 2006, pp. 413-416, 17-19 May 2006, Bucuresti;
- [10] Jazar R.N., Theory of Applied Robotics: Kinematics, Dynamics and Control (Second Edition), Springer, 2010;



- [11] Dombre E., Khalil W., Modelisation et commande des robots, Ed. Hermes, Paris, 1988;
- [12] Bădoiu D.G., On the Differential Model of a Mitsubishi Robot, Buletinul Universitatii Petrol-Gaze din Ploiesti, Seria Tehnica, Vol 64, No. 1, pp. 45-50, 2012;
- [13] Craig J.J., Introduction to Robotics: Mechanics and Control (Third Edition), Pearson Prentice Hall, 2005;
- [14] Bădoiu D., Research Concerning the Use of Polynomial Functions in the Study of the Conventional Sucker Rod Pumping Units, Revista de Chimie, vol. 70, nr. 4, pp. 1223-1227, 2019;
- [15] Bădoiu D., Research on establishing the differential model of the robotic mechanisms, Romanian Journal of Petroleum & Gas Technology, Vol. 3, No. 1, pp. 49-54, 2022;
- [16] Badoiu D., *Research concerning the static balancing of a multiloop linkage*, Romanian Journal of Petroleum & Gas Technology, Vol. 2, No. 1, 2021;
- [17] Badoiu D., On an Optimal Generation of the Trajectory in the Case of a Robotic Mechanism with Four Degrees of Freedom, Buletinul Universitatii Petrol-Gaze din Ploiesti, Seria Tehnica, vol. 69, nr. 1, pp. 31-36, 2017;
- [18] Bădoiu D., On the Establishing and Solving of the Movement Equation in the Case of the Plane Mechanisms, Buletinul Universitatii Petrol-Gaze din Ploiesti, Seria Tehnica, Vol 67, No. 3, pp. 87-93, 2015;
- [19] Bădoiu D., On the calculus of the equilibrium moment for a mechanism with three independent contours, Buletinul Universitatii Petrol-Gaze din Ploiesti, Seria Tehnica, Vol. 67, No. 1, pp. 99-104, 2015;
- [20] Sandor G. N., Erdman A. G., Advanced Mechanism Design: Analysis and Synthesis (Volume 2), Prentice-Hall Inc., Englewood Cliffs, New Jersey, USA, 1984;
- [21] Nikravesh P. E., *Computer-Aided Analysis of Mechanical Systems*, Prentice-Hall Inc., Englewood Cliffs, New Jersey, USA, 1988;
- [22] Zhang C., Yang J., Chang Z., Machinery dynamics, Academic Press, 2022;
- [23] Bădoiu D., On Determining the Solution of a Problem Concerning the Positioning and Orientation of the Lynx 6 Robot System, Buletinul Universitatii Petrol-Gaze din Ploiesti, Seria Tehnica, Vol 63, No. 3, pp. 15-18, 2011;
- [24] Bădoiu D., Analiza structurală si cinematică a mecanismelor, Editura Tehnică, Bucure sti, 2001;
- [25] Monagan M. B., Geddes K.O., Heal K.M., Labahn G., Vorkoetter S.M., Mccarron J., Demarco P., *Maple Introductory Programming Guide*, Maplesoft, a division of Waterloo Maple Inc., 2005.

Received: October 2024; Revised: October 2024; Accepted: November 2024; Published: November 2024